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THEORETICAL PRINCIPLES OF CALCULATING PARAMETERS AND AMPLITUDE OF VIBRATION OF BELT CONVEYOR ROLLER MECHANISMS OF STRAP ELEMENT BEARING SUPPORTS

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Abstract. The article presents ideas about the reliability and durability of belt conveyors in mining enterprises today, as well as the constantly increasing requirements for equipment. In order to increase the service life of the bearing supports of belt conveyor roller mechanisms, it was found that it is possible to increase the service life of the mechanisms by using rubber bushings on the outer side of the bearing. According to this, the analysis of scientific studies has been carried out that when bushings with belt elements are used in roller mechanisms, it is possible to increase the UWK compared to the traditional one due to the reduction of the amplitude of vibrations in it.

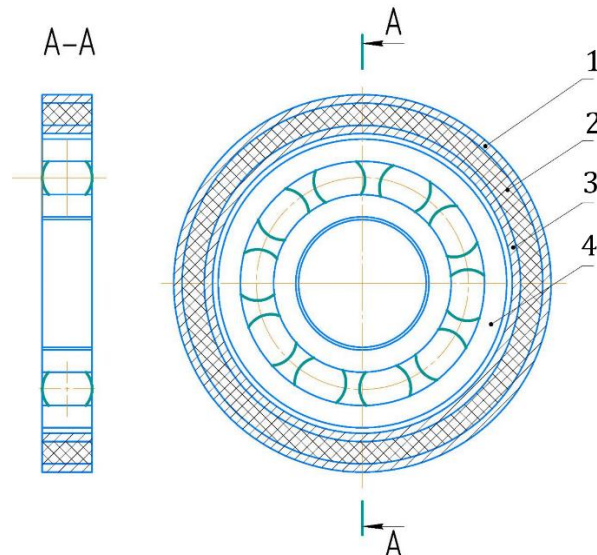
Keywords. Conveyor, roller mechanism, belt element, deformation, loading, transportation, amplitude, vibration, technology.

Today, belt conveyors are widely used in mining enterprises of our country and abroad, and they are significant for the fact that they have the highest performance compared to other means of transportation at a very low cost. In addition, this vehicle characterizes a high level of interaction with other types of technological machinery and equipment, which in turn increases the technical level of the production cycle and the work of the entire mining enterprise. has a positive effect on increasing efficiency.

One of the parts that determine the efficiency and periodicity of the belt conveyor is the guide roller mechanism. The durability and reliability of the guide roller mechanism is characterized by factors such as various loads (percussive and non-percussive), physical and mechanical properties. Depending on the operating conditions of the guide roller mechanism, the parts of rolling bearings are designed in different ways [1, 2].

During the operation of belt conveyor equipment, vibrations occur mainly in roller mechanisms. This, in turn, does not affect the support bearings of roller mechanisms. We can see that the vibrations change minimally when the roller mechanism of the new design with the belt element bearing support is used [3, 4].

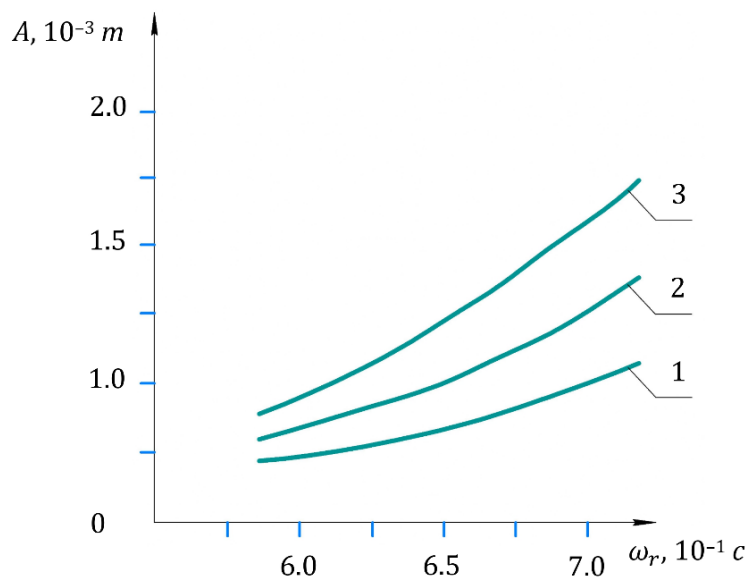
Centrifugal force ($350 \div 400$) N changes within the limit, taking into account the variation of $D_r = 0.4$ m at the rotation speed of $n = 450$ rev/min . It should be noted that the belt element changes proportionally to the load on the bearings of the roller mechanism. However, we can see that the deformation of the support changes in a non-linear state depending on the changes in the loads of cylindrical belt element bushings used as an outer cover for the roller mechanism support bearings (Fig. 1) [5-9].



1- outer ring; 2- bushing with belt element; 3- inner bushing; 4- bearing

Figure 1. Bearing support with elastic element (Roller mechanism)

Fig. 2 shows graphs of the dependence of the amplitude of the vibrations on the belt supports of the roller mechanisms and the change of the angular speed. In this case, the increase in the angular velocity of the roller mechanism causes its nonlinear vibration amplitude to hang. As a result, when changing from 68 c^{-1} to 80.2 c^{-1} , the amplitude of vibrations with the mass of the roller mechanism bearing shell and the outer flange of the belt element increases from $0.205 \cdot 10^{-3} \text{ m}$ to $0.61 \cdot 10^{-3} \text{ m}$. When the mass of the bearing shell is $m_{sh} = 0.5 \text{ kg}$ and the mass of the outer flange of the belt element is $m_f = 0.350 \text{ kg}$, the amplitude A increases from $0.42 \cdot 10^{-3} \text{ m}$ to $1.409 \cdot 10^{-3} \text{ m}$. The results of the experimental studies show that the vibration amplitude of the support of the roller mechanism with a belt element is in the range of $(0.3 \div 0.38) \cdot 10^{-3} \text{ m}$. To ensure these values, values $m_{sh} = (0.450 \div 0.5) \text{ kg}$, $m_f = (0.3 \div 0.350) \text{ kg}$ are recommended [10, 11].

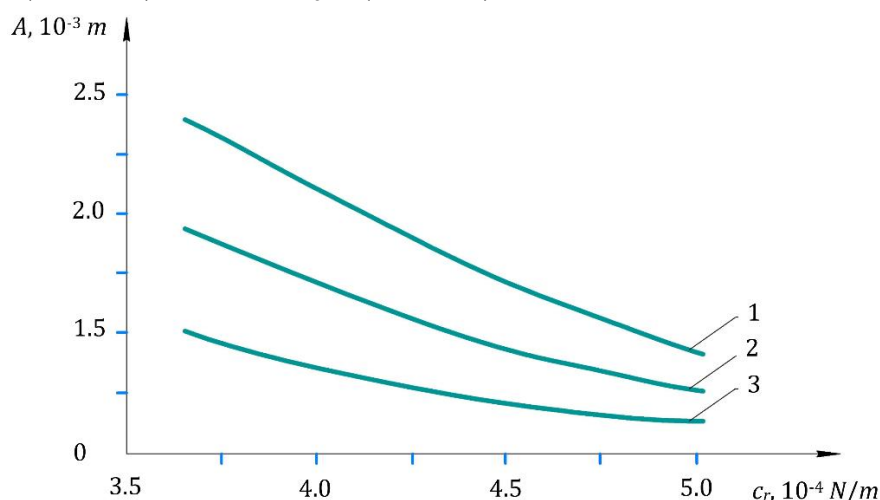


where, $1 - m_{sh} = 0.35 \text{ kg}$, $2 - m_{sh} = 0.45 \text{ kg}$, $3 - m_{sh} = 0.55 \text{ kg}$.

Figure 2. Graphs of the dependence of changes in the amplitude of vibrations on the belt supports of the roller mechanism and the change in angular speed

Fig. 3 shows graphs of the dependence of the variation of the vibration amplitude of the pulley mechanism on the variation of the stiffness coefficient of the supports with strap elements. The given graphic correlation graphs show that as the coefficient of friction of the belt element bearing support increases from $4.64 \cdot 10^4 \text{ N/m}$ to $6.2 \cdot 10^4 \text{ N/m}$, the vibration amplitude of the roller mechanism decreases from $1.317 \cdot 10^{-3} \text{ m}$ to $0.42 \cdot 10^{-3} \text{ m}$ it decreases linearly up [12-14].

To ensure that the vibration amplitude of the roller mechanism is in the range of $(0.3 \div 0.38) \cdot 10^{-3} m$ $c = (5.2 \div 6.0) 103 N/m$; $\omega_c = (7.2 \div 7.6) 10 c^{-1}$; It is recommended that $k = 0.3 \div 0.5$.



where, $1 - k = 0.6$; $\omega_c = 80 c^{-1}$; $2 - k = 0.4$; $\omega_c = 76 c^{-1}$; $1 - k = 0.2$; $\omega_c = 70 c^{-1}$;

Figure 2. Graphs of dependence on changes in the vibration amplitude of the roller mechanism

Summary. The influence of the parameters of belt conveyor roller mechanisms and the coefficient of uniformity of the bearing support with belt elements on the amplitude of vibrations was studied. Calculations were made to calculate the amplitude and frequency of vibrations of the roller mechanism, as well as the dynamic coefficient of the system, and graphs of its dependence were developed. In order to ensure the vibration of roller mechanisms in certain intervals, the recommended values were developed taking into account the support of the bearing with the belt element.

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